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-TECHNICAL REPORT---

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THE NATION'S LABORATORY FOR ADVANCED AUTOMOTIVE TECHNOLOGY



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Computer Generated Root-Mean-Square (RMS) Roughness Courses for Ride Quality **Evaluation**

> Wesley W. Bylsma $\mathbf{B}\mathbf{y}$

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U.S. Army Tank-Automotive Research, Development, and Engineering Center **Detroit Arsenal** Warren, Michigan 48397-5000

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by Wesley W. Bylsma

U.S. Army Tank-automotive and Armaments Research, Development and Engineering Center ATTN: AMSTA-TR-R/159 Warren, MI 48397-5000

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1. ABSTRACT

This report presents a suite of root-mean-square (RMS) computer generated ride quality courses in the range of 0.10 to 5.00 inches RMS for use in evaluating vehicle dynamics by computer simulation.

Power Spectral Density descriptions of each surface profile were used with digital simulation of stationary random processes to generate distance histories. Theoretical foundations and background on random processes and analysis of them are referenced.

For the specific example of surface profiles the mathematical preliminaries demonstrated the particular analytical techniques necessary to simulate random processes and apply it to surface profiles. In our examples the surface profile description was a one sided power spectral density function with defined constant slope frequency domain.

With the ability to simulate surface profiles and the -2 (log scale) slope description restriction the constant c was determined relating the surface roughness parameter, RMS, to the PSD surface profile description, allowing for the generation of a set of courses to simulate any desired level of surface roughness.

2. INTRODUCTION

One of the driving forces in evaluating vehicle dynamics is the surface profile. Simulations of vehicle dynamics are used to predict system performance based on human tolerance limits to vibration levels over a specified roughness course.

Descriptions of surface profiles have been presented in Van Deusen (1967), Dodds and Robson (1973), Healey et.al. (1977). A generalized case for relating random processes to surface profiles is addressed in Shinozuka (1971).

Computer generation of these RMS roughness courses is based on the simulation of stationary random processes, by which the designer can define the type of surface profile desired through frequency content and generate a time series.

2.1 Random Processes

Random processes are used to mathematically represent a surface profile since naturally occurring surfaces are not predefined and depending on the current geographical area do have variability in them. Naturally occurring phenomenon

and environmental conditions, such as rain, wind, snow, and temperature fluctuations cause changes to occur. For in-depth coverage of random processes Papoulis (1984) is highly recommended.

2.2 Power Spectral Density

To generate roughness courses the fundamental relationship between the Power Spectral Density (PSD) function, $S_g(w)$, and the distance domain,

g(x), needs to be found where the PSD is the Fourier Transform of the auto-correlation function

$$S_g(w) = \frac{1}{2\pi} \int_{-\infty}^{+\infty} R_g(\tau) e^{-jw\tau} d\tau$$
 (1)

and the auto-correlation function can be gotten from the PSD through the inverse Fourier Transform

$$R_{g}(\tau) = \int_{-\infty}^{+\infty} S_{g}(w)e^{jw\tau}dw$$
(2)

where

$$R_g(\tau) = E[g(x+\tau)g^*(x)]$$
(3)

with $E[\]$ being defined as the standard expectation operator. For real-valued random processes the autocorrelation function is even which reduces the PSD to

$$S_{g}(w) = \int_{-\infty}^{+\infty} R_{g}(\tau) \cos(w\tau) d\tau.$$
 (4)

giving a real-valued, even PSD of w.

2.3 Random Process Simulation

Simulation of the random process requires the use of the relationship between the surface profile function g(x) and the PSD function $S_g(w)$. The forward operation

$$g(x) \to S_g(w)$$
 (5)

known as the PSD is defined in (1). Proakis and Manolakis (1988) discuss many well known methods for calculating PSD's. Less obvious is the reverse operation

$$S_g(w) \to g(x)$$
. (6)

The difficulty lies in that g(x) is in terms of the auto-correlation function. A direct extraction of g(x) from $R_g(\tau)$ is problematic.

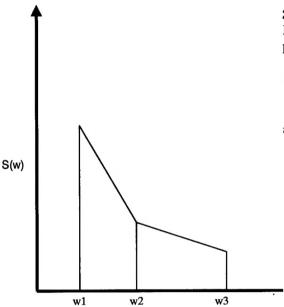


Figure 1 - Example Power Spectral Density function

From (2) and (3) the expected value relates the distance function to the PSD identifying a relationship that will satisfy (6). Through the use of trigonometric identities and conveniently chosen probability distributions Shinozuka and Jan (1972) determined the relationship to be

$$g(x) = \sqrt{2} \sum_{k=1}^{N} \sqrt{S_g(w_k) \Delta w_k} \cos(w_k' x + \phi_k)$$
(7)

where ϕ is a random phase angle uniformly distributed between 0 and 2π ,

$$\Delta w_k = \frac{w_{upper} - w_{lower}}{N}$$
 with $w_{wpper} = w_3$ and

 $W_{lower} = W_1$ as depicted in Figure 1,

$$W_k = W_{lower} + (k - 0.5)\Delta W_k$$
, and

 $w'_k = w_k + \delta w$ where δw is uniformly distributed

between
$$\frac{-\Delta w'_k}{2}$$
 and $\frac{+\Delta w'_k}{2}$ where

 $\Delta w_k' \ll \Delta w_k$ to avoid periodicity.

Equation (7) assumes a zero mean, both in ensemble average and temporal mean. Shinozuka and Jan (1972) detail the theoretical basis for these requirements and show the applicability of this

method to the multi-dimensional case.

2.4 Generation of Surface Profiles

It is generally accepted that the PSD of a surface profile can be represented as

$$S_{g}(w) = \begin{cases} c_{1}w^{-n_{1}}, & w_{1} \leq w < w_{2} \\ c_{2}w^{-n_{2}}, & w_{2} \leq w < w_{3} \end{cases}$$
(8)

as shown in Figure 1.

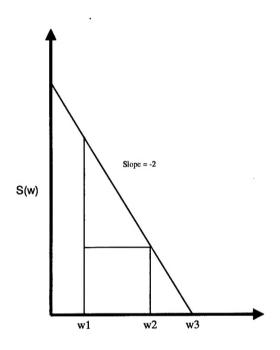


Figure 2 - Example Power Spectral Density function with constant -2 slope

As noted by Sevin and Pilkey (1971) most surfaces can be approximated by

$$S_g(w) = cw^{-2}, \ w_1 \le w < w_3$$
 (9)

alone. For this special case note the logarithmic plot is

$$\log(S_g(w)) = -2\log(w) + \log(c) \tag{10}$$

which produces a straight line with slope of -2 as shown in Figure 2.

Further, Parseval's Theorem states that the variance of g(x) is the area under $S_g(w)$. An often used measure of surface roughness is the root-mean-square (RMS) value

$$RMS = \sqrt{\frac{1}{L} \int_0^L g(x)^2 dx} = \sigma$$
(11)

which is the standard deviation, σ , or the square-root of the variance for zero-mean g(x). Given the -2 slope assumption in (10) and using Parseval's Theorem c is directly related to RMS by

$$c = (RMS)^2 \frac{w_1 w_2}{(w_2 - w_1)}.$$
(12)

For various levels of RMS roughness the corresponding c can be found and used to define the PSD from Figure 2 which, when simulated, will produce a course with the desired roughness.

The more general case in (8) adds flexibility to the surface profile description of the PSD which it estimates, although it has been found that (9) can give a good approximation to the PSD within a band of +/-3dB.

Ashmore and Piersol (1997) have determined surface profiles based on the definition in (9) for military and commercial roads.

3. RESULTS

The following pages show figures of the generated surface profiles from 0.10 to 5.00 inch RMS in 0.1 increments. Each is 1000 feet with 3 inch samples (4000 points). Each contains the PSD plot with original surface profile description, $S_g(w)$, between +/- 3dB bands and circle points of the PSD generated from g(x) in the first pane. The second pane is a sectional plot of g(x), with the third pane containing a histogram of the full signal. Dimensional units are

not included with the plots but are in $\frac{ft^2}{1/ft}$ for

 $S_g(w)$ and ft for g(x). The shape of the histogram should be noted as that of a Gaussian distribution, with parameters of μ =0, the mean, and σ , the standard deviation. This should not be surprising since the Central Limit Theorem of random variables applies from the summation in (7). Increased RMS levels are also shown by the spread out histogram which corresponds to greater σ since the area of $S_g(w)$ is related to RMS through Parseval's Theorem.

For each RMS level (0.10 - 5.00) inches in 0.1 increments) ten surface profiles g(x) were generated. Figures 3-52 show only one of these for each RMS level. Figures 53-102 are plots of each profile in its entirety with units of inches versus feet. Figures 103-105 show the comparative RMS level between 1.00, 3.00, and 5.00 inch RMS courses all plotted on the same scale (-20 to 20 inches). For reasons of brevity, an example listing of the surface profile (5.00) file is included for reference purposes. Each file is in American Standard Code for Information Interchange (ASCII) with the following format:

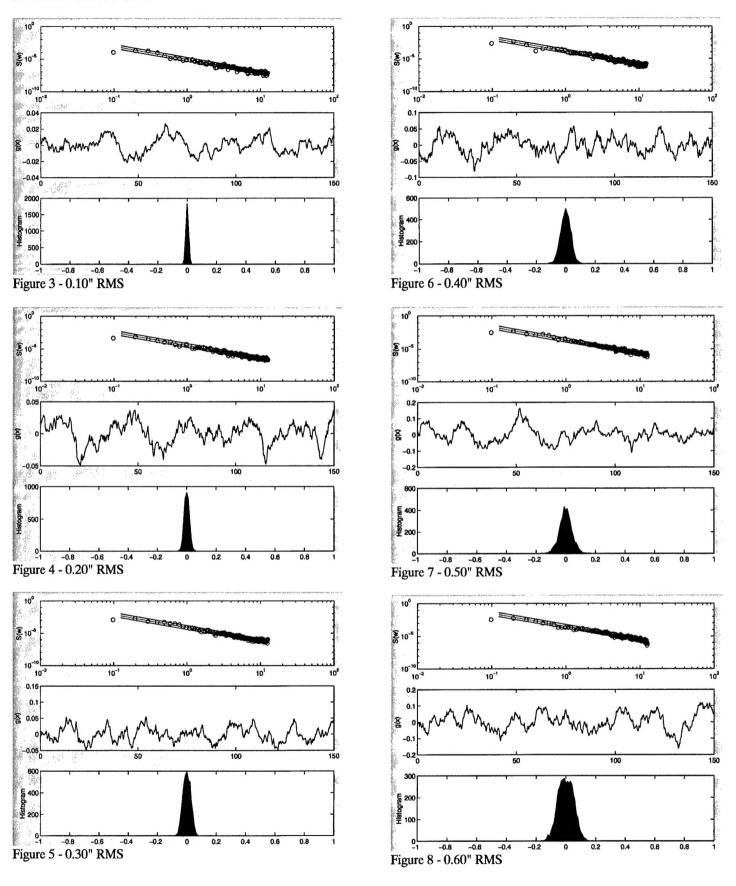
```
---BOF---
label
length (points), spacing (inches)
elevation point #0 (inches)
elevation point #1 (inches)
.
.
.--EOF---
```

Below is a specific example.

```
---BOF---
RMS ROUGHENESS COURSE 1
4000, 3.0
0.0123
0.1236
-0.0900
.
```

For each elevation point the distance is point#*spacing (starting at zero).

3.1 RMS Course PSD's



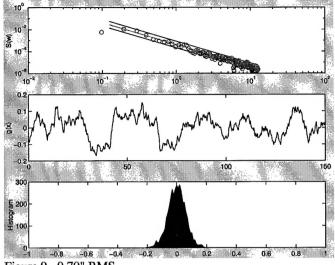


Figure 9 - 0.70" RMS

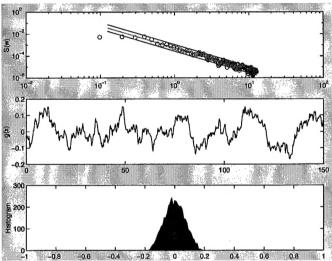


Figure 10 - 0.80" RMS

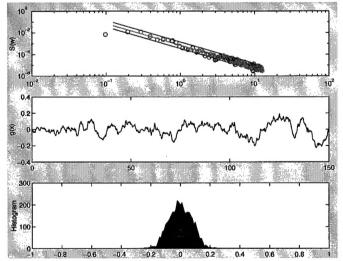


Figure 11 - 0.90" RMS

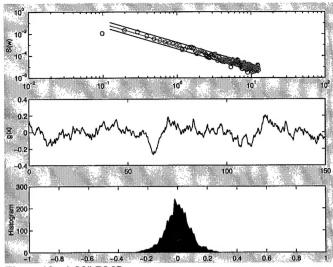
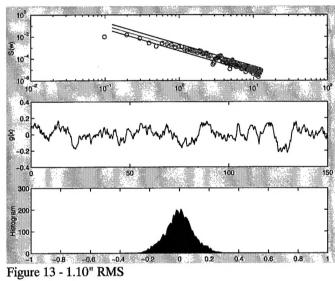


Figure 12 - 1.00" RMS



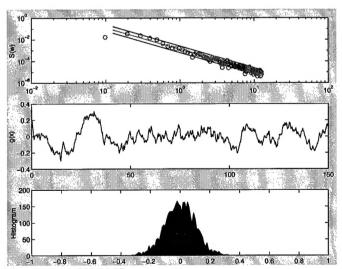
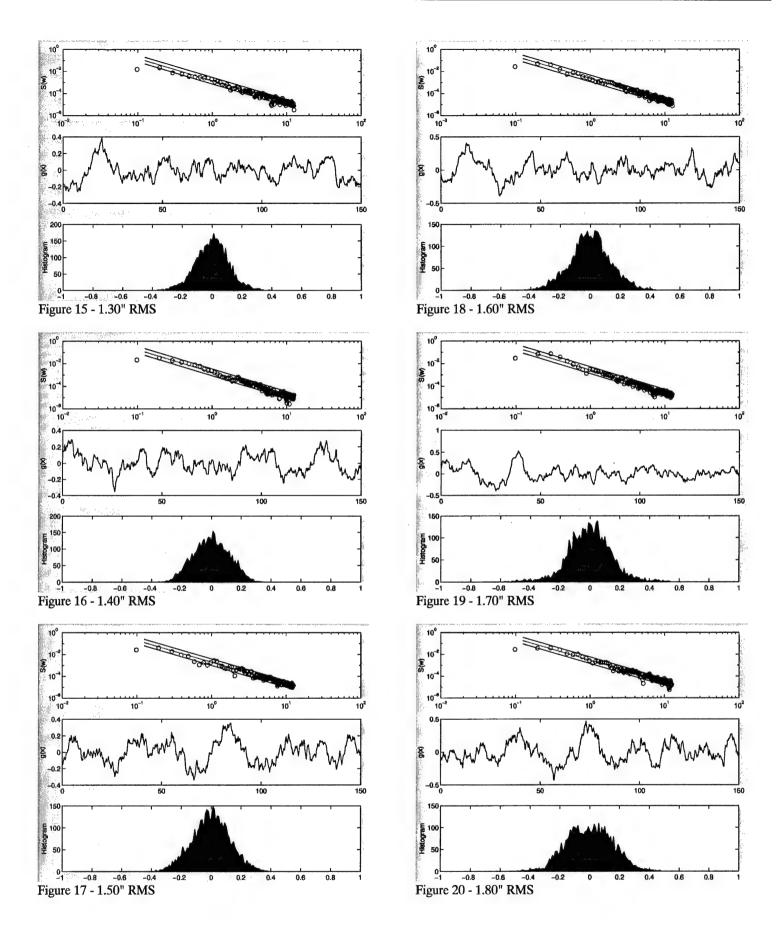
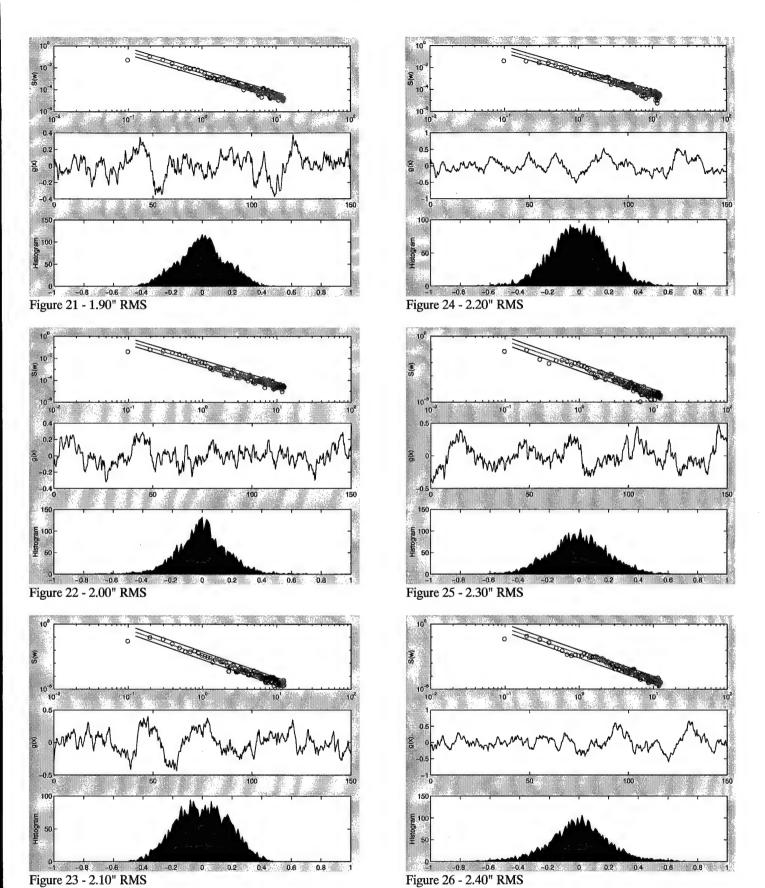
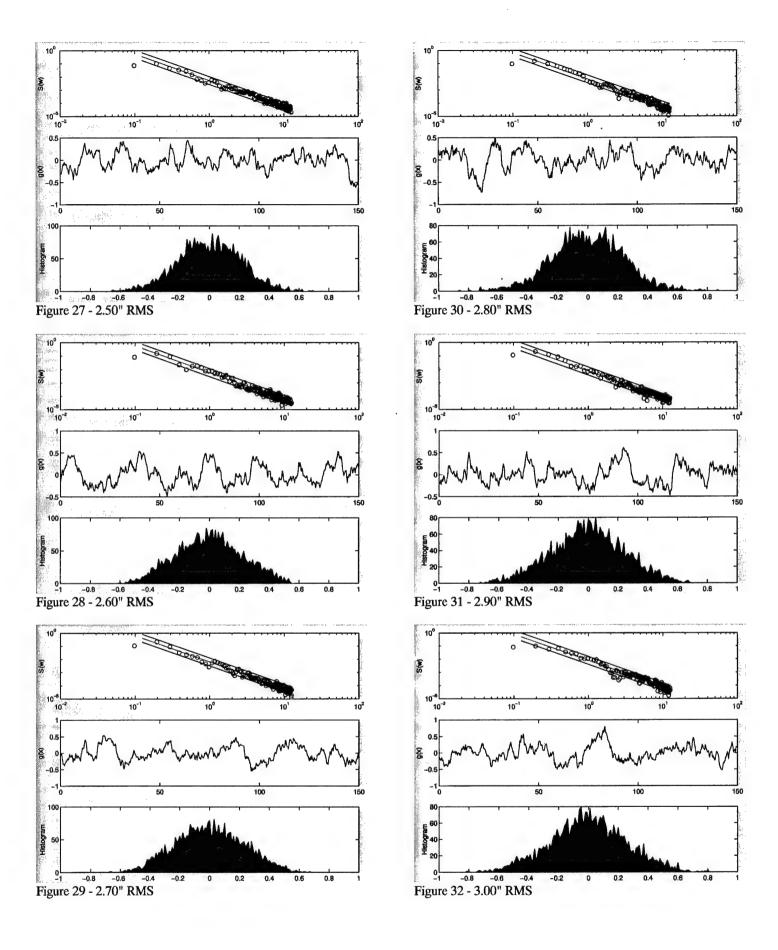


Figure 14 - 1.20" RMS







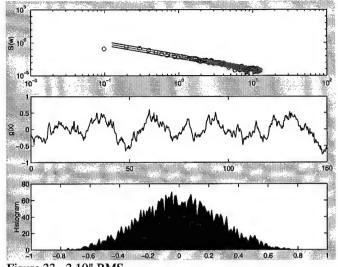
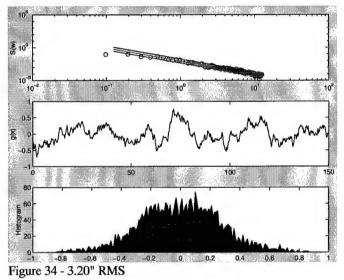


Figure 33 - 3.10" RMS



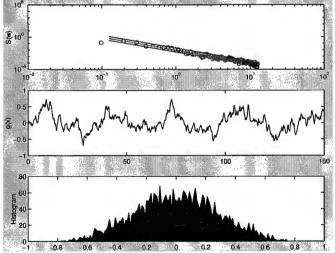
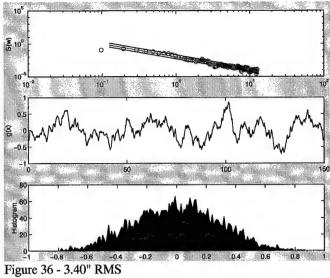
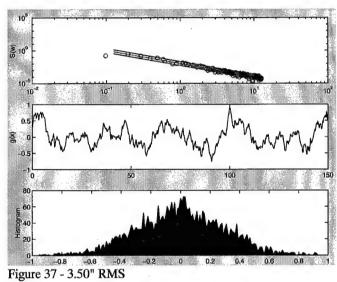


Figure 35 - 3.30" RMS





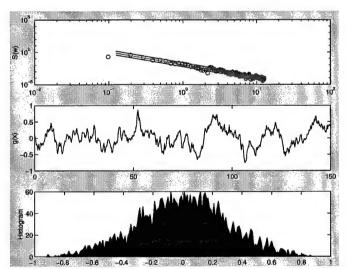
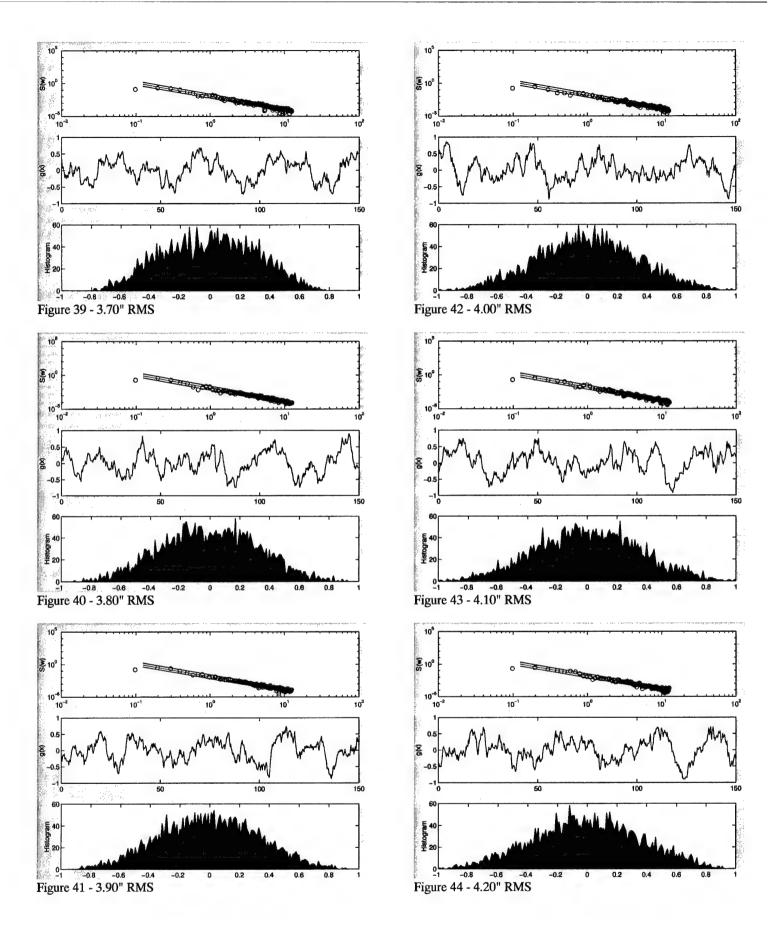
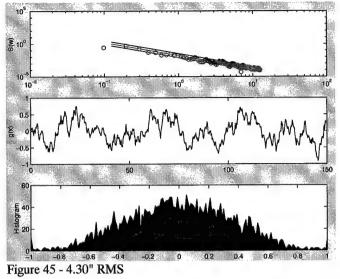
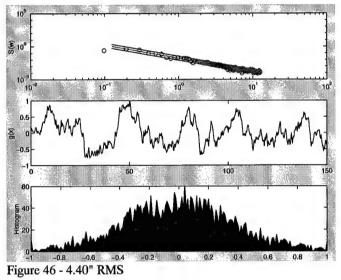


Figure 38 - 3.60" RMS







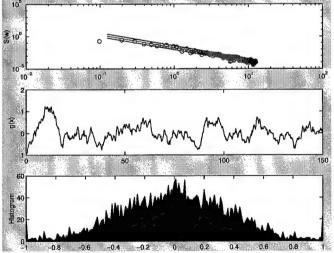
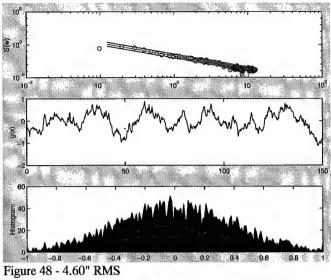
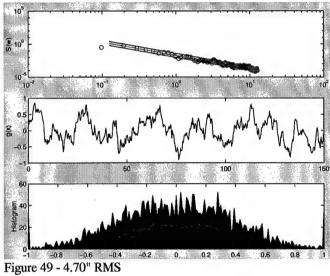
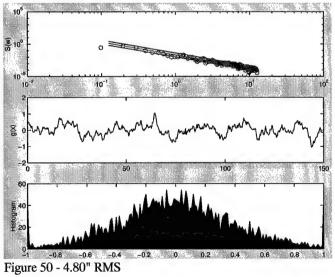
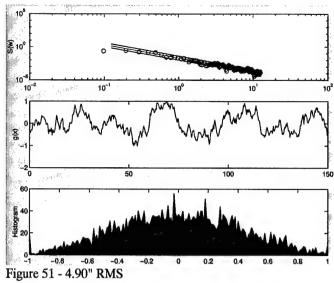


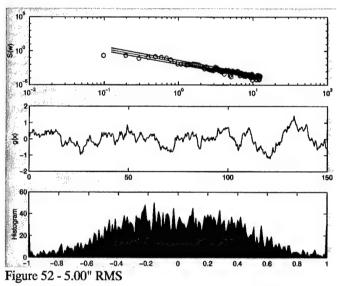
Figure 47 - 4.50" RMS











3.2 Full RMS Course Plots

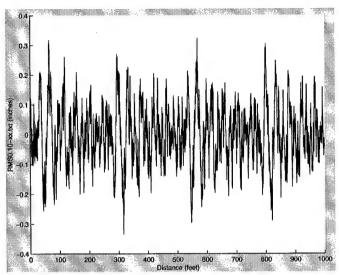


Figure 53 - 0.10" RMS

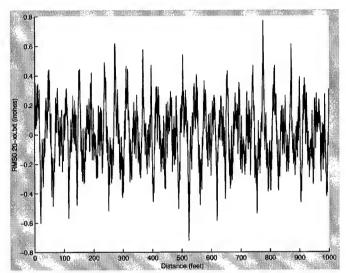


Figure 54 - 0.20" RMS

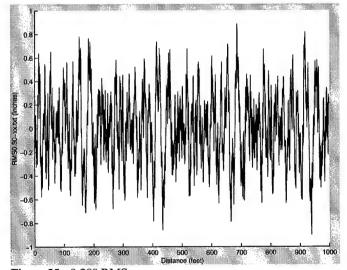


Figure 55 - 0.30" RMS

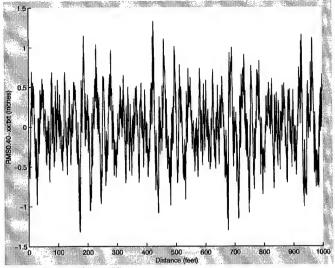


Figure 56 - 0.40" RMS

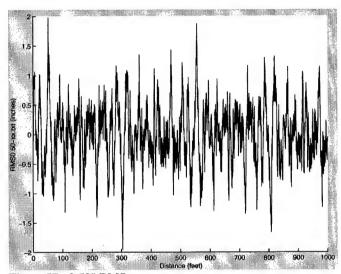


Figure 57 - 0.50" RMS

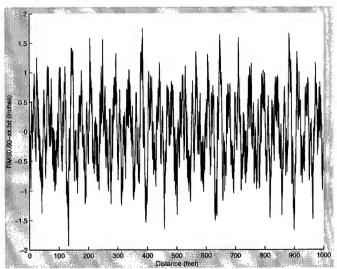
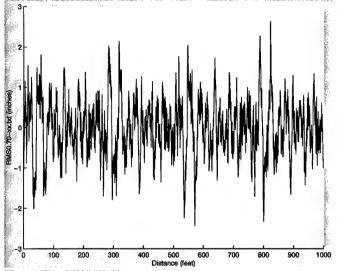
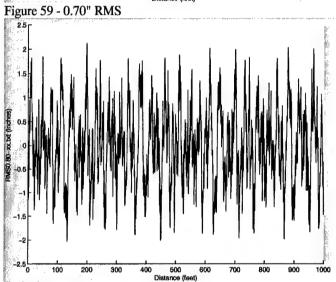
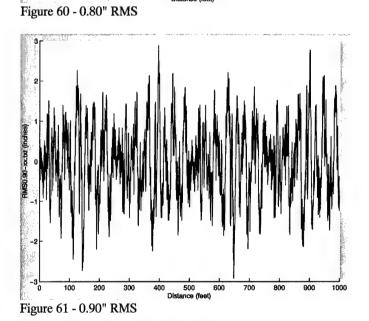


Figure 58 - 0.60" RMS







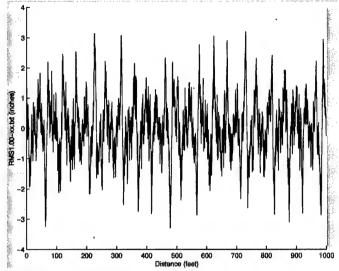


Figure 62 - 1.00" RMS

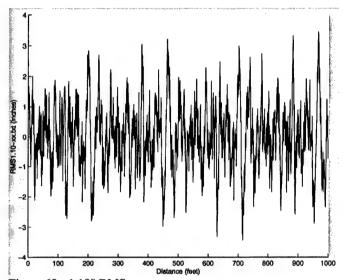


Figure 63 - 1.10" RMS

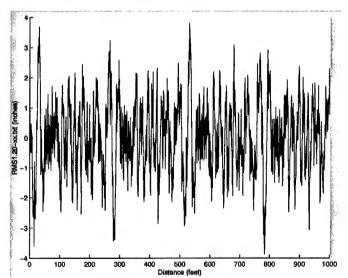


Figure 64 - 1.20" RMS

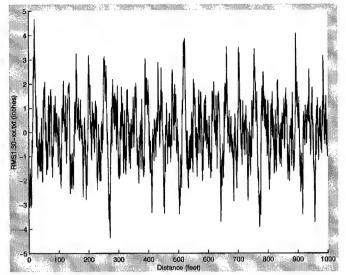


Figure 65 - 1.30" RMS

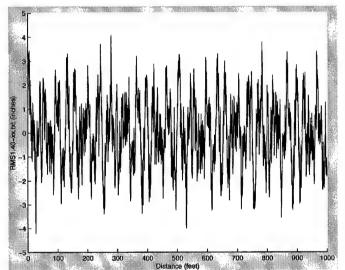


Figure 66 - 1.40" RMS

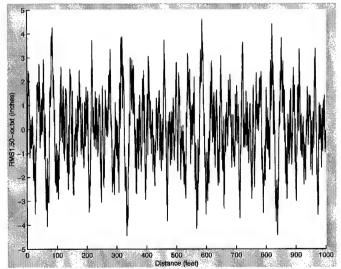


Figure 67 - 1.50" RMS

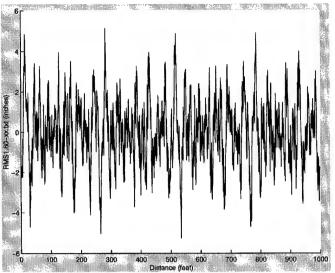


Figure 68 - 1.60" RMS

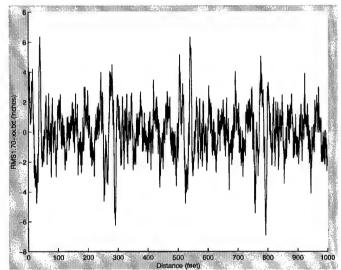


Figure 69 - 1.70" RMS

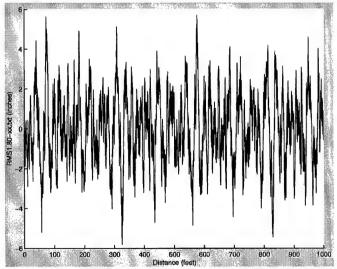


Figure 70 - 1.80" RMS

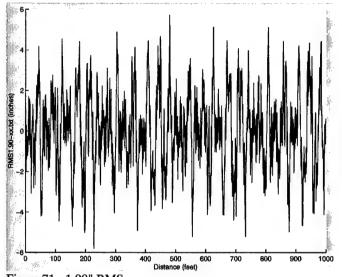


Figure 71 - 1.90" RMS

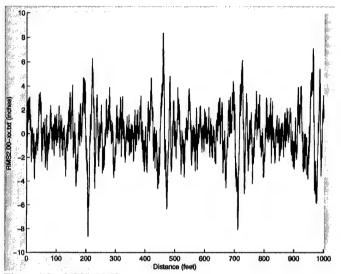


Figure 72 - 2.00" RMS

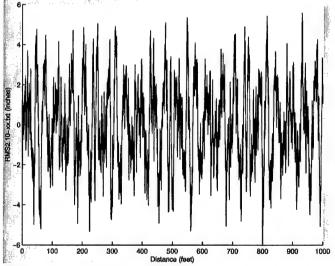


Figure 73 - 2.10" RMS

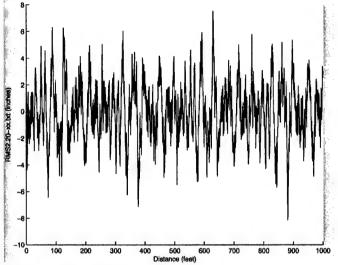


Figure 74 - 2.20" RMS

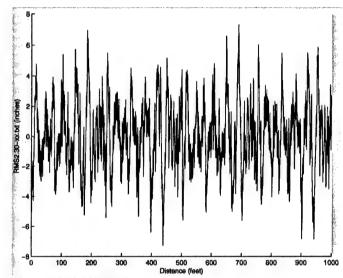


Figure 75 - 2.30" RMS

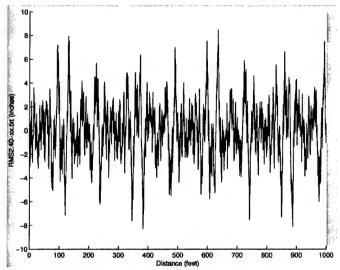


Figure 76 - 2.40" RMS

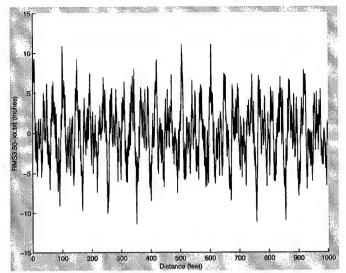


Figure 77 - 2.50" RMS

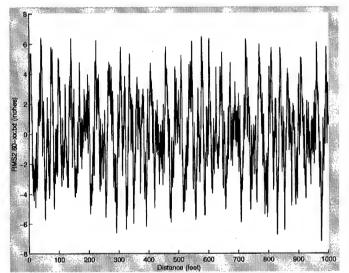


Figure 78 - 2.60" RMS

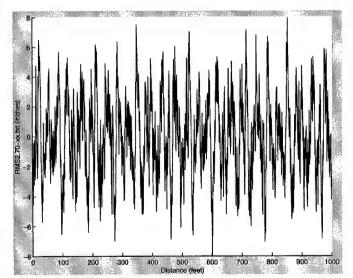


Figure 79 - 2.70" RMS

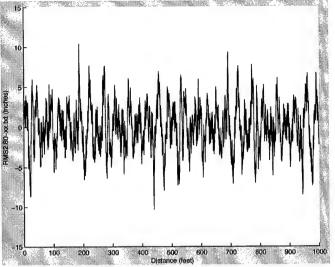


Figure 80 - 2.80" RMS

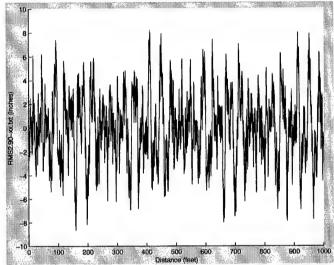


Figure 81 - 2.90" RMS

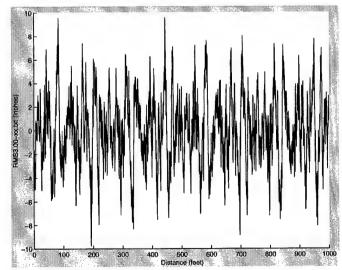


Figure 82 - 3.00" RMS

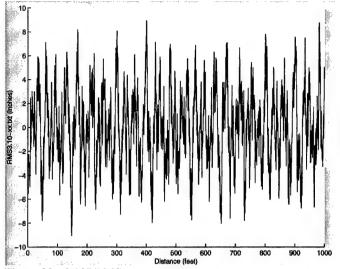


Figure 83 - 3.10" RMS

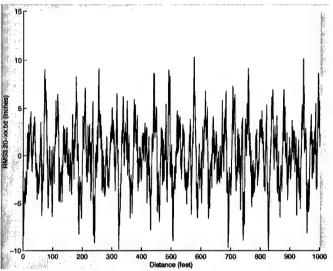


Figure 84 - 3.20" RMS

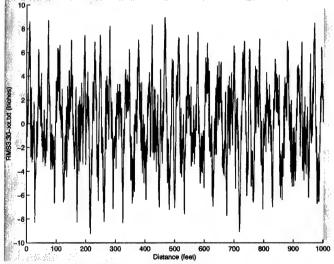


Figure 85 - 3.30" RMS

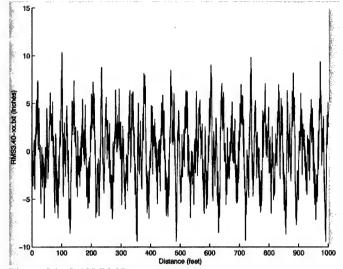


Figure 86 - 3.40" RMS

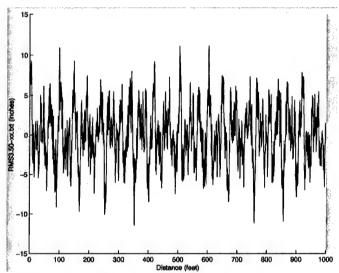


Figure 87 - 3.50" RMS

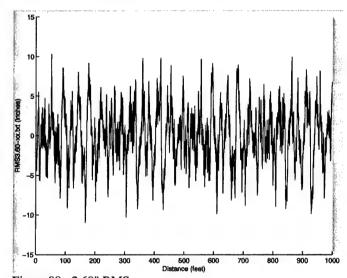


Figure 88 - 3.60" RMS

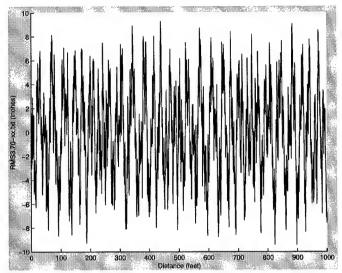


Figure 89 - 3.70" RMS

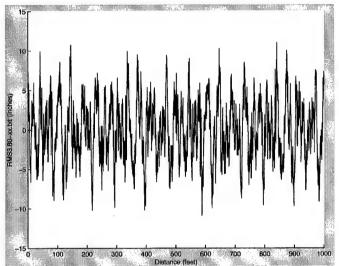


Figure 90 - 3.80" RMS

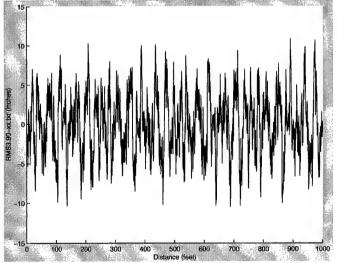


Figure 91 - 3.90" RMS

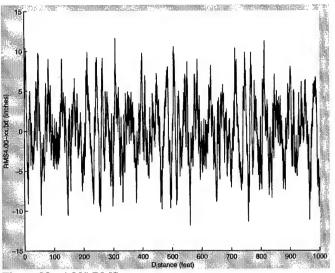


Figure 92 - 4.00" RMS

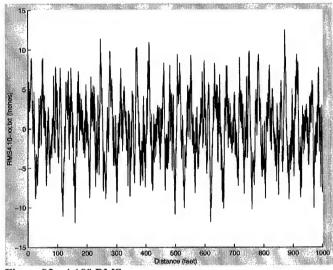


Figure 93 - 4.10" RMS

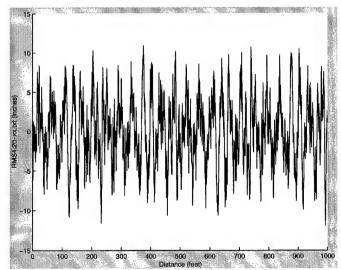
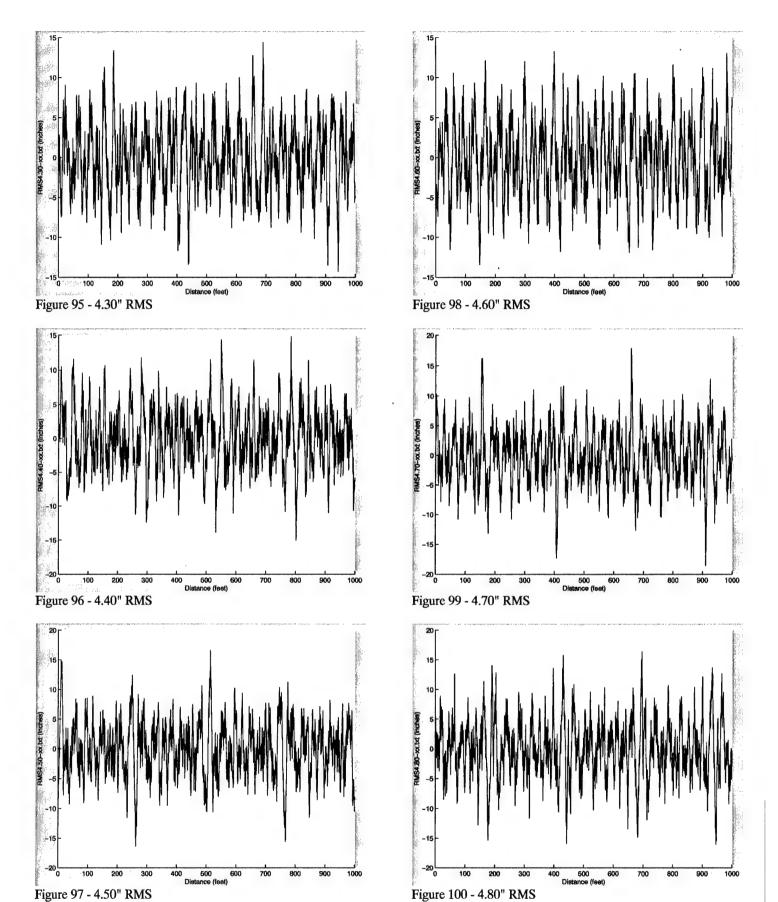
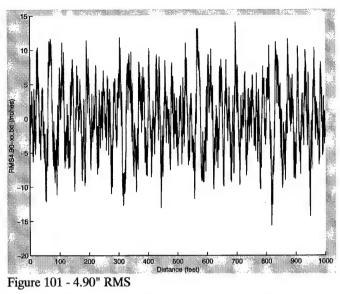


Figure 94 - 4.20" RMS





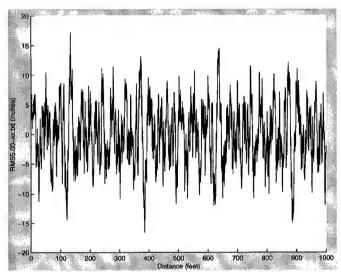
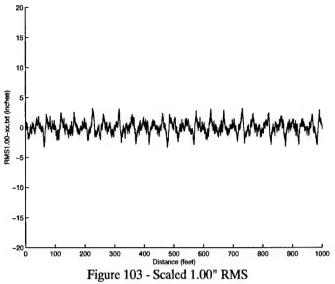
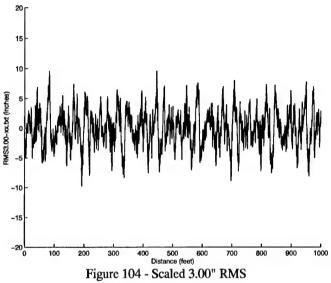
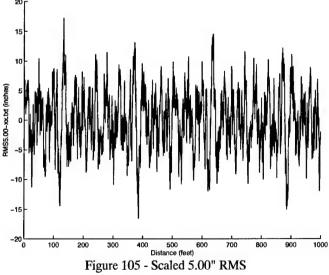


Figure 102 - 5.00" RMS







3.3 RMS Course Listing Example 7.403425 5.472385 5.463148 6.088272 7.202758 6.745740 3.830878 2.299082 1.877482 2.534675 .667419 .955772 .446484 .239576 .741907 .659139 .127577 .804318 .745477 .404248 -6.333341 -5.763155 -6.499456 -8.032326 5.642677 -2.777471 2.624828 332385 013225 0.637901 4.362432 .909815 .345447 218093 .983325 596493 105487 .510880 .336033 -3.637611 -5.853110 .265635 323324 931356 235779 318767 -5.853110 -5.650797 -2.701498 -5.034795 -5.357788 -4.737441 -5.492590 -4.590536 -4.282752 -2.711306 /magnitude 944331 166833 808378 520398 . 233902 . 393708 . 423254 .017086 .554206 .901053 .076538 786929 480711 079977 240821 .520398 .569646 .454334 .657194 .431590 .301497 .360488 .002372 .290645 .805955 4000, 3.000000 343440 343440 0.616628 1.294620 406534 416479 134897 .232372 240821 828401 172338 470246 134906 ..735384 ..215770 ..448553 1.972339 1.239255 1.291829 1.244792 1.643449 1.074436 1.462690 3.486668 2.240444 3.217577 3.080462 1.753535 0.877995 3.34550 6.39917 8.36499 9.540461 0.27660 1.106454 1.699111 4.480530 4.536882 4.798883 4.353879 4.490341 6.713574 6.079264 .797762 .283610 .084014 .550317 .939657 .810707 251142 559396 3.311299 3.800252 . 137958 897043 364720 437960 .507172 519191 0.209765 813537 .043896 .686219 535547 5.691117 4.937887 932410 .903626 349904 5.724641 3.875455 521802 .168450 .340269 .349904 .386170 .643335 .130691 0.565466 3.864389 4.290983 5.404745 6.724727 6.095410 .521802 .489776 .419319 .641501 .057454 .896720 .379957 .340269 .624617 .235179 .232424 .681644 .258456 .408453 .730841 .595334 .053036 .596694 .608038 .032337 .724507 687142 143024 422205 462694 3.002952 5.636799 4.674260 2.474602 681819 470558 5.884863 6.792294 .421873 .110911 .898653 0.583506 0.776313 2.488959 3.567192 6.292329 3.838150 773306 834180 .110911 .096924 .002130 .812004 .299452 .701340 .731272 .242121 .815674 .859728 .581011 .829540 .810102 701029 6.316228 6.812938 7.501085 7.441233 6.435994 5.801977 8.164461 8.591745 8.476425 .485317 .988532 .075987 .700249 .894969 .888289 .907253 852696 3.962392 452288 111188 733857 216590 433191 228420 .788531 .232365 . 142156 157459 4 026465 851914 911861 .660584 .911861 .188200 .547658 .735983 .605317 .166163 .563337 .215215 .917860 .101641 .352852 .652707 .551354 3.386198 . 848448 772500 813358 .813358 .366735 .797564 .250268 .510773 .664594 .838962 .949845 .096946 935515 211532 736243 3.20978 326963 572274 5.551354 6.070080 5.502972 3.227948 3.597680 4.916103 3.908908 3.913769 4.354650 2.172119 1.903586 5.164127 .068825 .262141 .495231 .183247 .119177 .974288 .759931 52751 .097250 275443 2.433056 1.217636 .275443 .939572 .254886 .412966 .849841 .188187 .013012 .468874 .813624 .815480 .069990 .905413 .067644 417358 223741 .009438 .958155 008658 785461 144579 037190 662683 460554 907743 993039 2.955834 1.066049 1.967376 457457 .410122 . 284037 . 860584 . 099346 . 005110 . 759035 .249363 406923 1.563290 0.461892 .400773 .210156 .379161 .991548 .829521 .853668 383423 575338 .495503 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677514 418808 998553 957671 022210 906505 053623 .845670 .616497 616175 0.282203 .229027 0.279762 0.105784 1.595251 417510 488701 889484 200014 558607 977437 .053623 .821280 .734516 .203231 .016652 1.851879 3.271280 .563969 .561611 .632550 .234255 0.807272 0.159976 41494 592999 204612 -1.68425--4.79485--1.82077) 0.615235-1.25642--0.080991 1.304907 2.200722-2.137996 0.816316 3.714922-4.181527 4.11162 4.502055-2.461430 0.956456-0.956456-0.77680-0.77680-2.77292-2.617924 3.207974 65029 2.327366 .904375 .934749 .310742 .062370 .374329 1.071604 0.054097 .941197 .355329 .277144 .718102 .822962 2.650295 2.802845 1.464372 -0.409812 0.003585 1.648306 3.036310 3.662153 3.290875 .467787 .806256 .762643 .542396 127413 237893 .092255 .542396 .050865 .895381 .553949 .078230 .766152 .041163 .602895 .237893 .566090 .526396 .452428 .817442 .381455 .269784 .449081 -2.092255 -1.805485 -3.202298 -5.991008 -5.248348 -5.476813 -3.941913 545885 68349 .19270 .109013 .723790 .916359 459499 985798 662289 837925 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1.86205 2.894272 3.590101 160230 .585851 .507072 .803002 .072676 .400653 0.248912 .069867 .806145 .374414 .639671 .716709 1.517803 1.745017 1.074015 1.091856 0.225956 0.209557 791969 765370 .163789 .765370 .961600 .860774 .036511 .949922 .176394 .685987 .579069 .059580 467673 593256 214922 0.039716 1.937009 139067 .593256 .858705 .915717 .930916 .552123 986592 255661 .799071 .586404 836563 577424 427180 403830 645196 . 166865 . 726826 . 557016 417526 . 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